

Institute for Interlaboratory Studies

> Results of Proficiency Test Bitumen November 2022



Author:ing. C.M. Nijssen-WesterCorrectors:ing. R.J. Starink & Mrs. E.R. Montenij-BosApproved by:ing. A.S. Noordman-de Neef

Report: iis

iis22F02

March 2023

CONTENTS

| 1 | | 3 |
|-----|---|----|
| 2 | SET UP | 3 |
| 2.1 | QUALITY SYSTEM | 3 |
| 2.2 | PROTOCOL | 3 |
| 2.3 | CONFIDENTIALITY STATEMENT | 3 |
| 2.4 | SAMPLES | 4 |
| 2.5 | STABILITY OF THE SAMPLES | 4 |
| 2.6 | ANALYZES | 4 |
| 3 | RESULTS | 5 |
| 3.1 | STATISTICS | 5 |
| 3.2 | GRAPHICS | 6 |
| 3.3 | Z-SCORES | 6 |
| 4 | EVALUATION | 7 |
| 4.1 | EVALUATION PER TEST | 7 |
| 4.2 | PERFORMANCE EVALUATION FOR THE GROUP OF LABORATORIES | 9 |
| 4.3 | COMPARISON OF THE PROFICIENCY TEST OF NOVEMBER 2022 WITH PREVIOUS PTS | 10 |

Appendices:

| 1. | Data, statistical and graphic results | 12 |
|----|---------------------------------------|----|
| 2. | Number of participants per country | 26 |
| 3. | Abbreviations and literature | 27 |

1 INTRODUCTION

Since 2014 the Institute for Interlaboratory Studies (iis) organizes a proficiency scheme for the analysis of Bitumen in accordance with the latest version of EN12591 Paving Grade every year. During the annual proficiency testing program 2022/2023 it was decided to continue the round robin for the analysis of Bitumen.

In this interlaboratory study 47 laboratories in 27 countries registered for participation, see appendix 2 for the number of participants per country. In this report the results of the Bitumen proficiency test are presented and discussed. This report is also electronically available through the iis website www.iisnl.com.

2 SET UP

The Institute for Interlaboratory Studies (iis) in Spijkenisse, the Netherlands, was the organizer of this proficiency test (PT). Sample analyzes for fit-for-use and homogeneity testing were subcontracted to an ISO/IEC17025 accredited laboratory. It was decided to send one sample of Bitumen grade 35/50 in a 2.5 liter can labelled #22240. The participants were requested to report rounded and unrounded test results. The unrounded test results were preferably used for statistical evaluation.

2.1 QUALITY SYSTEM

The Institute for Interlaboratory Studies in Spijkenisse, the Netherlands, has implemented a quality system based on ISO/IEC17043:2010. This ensures strict adherence to protocols for sample preparation and statistical evaluation and 100% confidentiality of participant's data. Feedback from the participants on the reported data is encouraged and customer's satisfaction is measured on a regular basis by sending out questionnaires.

2.2 PROTOCOL

The protocol followed in the organization of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of June 2018 (iis-protocol, version 3.5). This protocol is electronically available through the iis website www.iisnl.com, from the FAQ page.

2.3 CONFIDENTIALITY STATEMENT

All data presented in this report must be regarded as confidential and for use by the participating companies only. Disclosure of the information in this report is only allowed by means of the entire report. Use of the contents of this report for third parties is only allowed by written permission of the Institute for Interlaboratory Studies. Disclosure of the identity of one or more of the participating companies will be done only after receipt of a written agreement of the companies involved.

2.4 SAMPLES

A batch of 70 subsamples of Bitumen grade 35/50 in 2.5 L metal cans was obtained from a local supplier and labelled #22240.

The homogeneity of the subsamples was checked by determination of Penetration at 25 °C in accordance with EN1426 and Softening Point in accordance with EN1427 on 4 stratified randomly selected subsamples.

| | Softening Point (Ring and Ball) in °C | Penetration in 0.1 mm |
|-----------------|--|--------------------------|
| sample #22240-1 | 54.4 | 44 |
| sample #22240-2 | 54.4 | 44 |
| sample #22240-3 | 55.0 | 44 |
| sample #22240-4 | 54.4 | 45 |

Table 1: homogeneity test results of subsamples #22240

From the above test results the relative standard deviations (RSD) were calculated and compared with 0.3 times the corresponding average relative standard deviation obtained from two iis PTs with grade 35/50 Bitumen conducted in 2018 and 2020 in agreement with the procedure of ISO13528, Annex B2 in the next table.

| | Softening Point (Ring and Ball) | Penetration |
|-------------------------------|---------------------------------|-------------|
| RSD% (observed) | 0.5 | 1.1 |
| reference method | iis PTs | iis PTs |
| 0.3 x RSD% (reference method) | 0.4 | 2.0 |

Table 2: evaluation of the repeatability of subsamples #22240

The calculated relative standard deviations are in agreement with 0.3 times the corresponding average relative standard deviation obtained from the previous iis PTs. Therefore, homogeneity of the subsamples was assumed.

To each of the participating laboratories one 2.5 L can of sample #22240 was sent on November 8, 2022. An SDS was added to the sample package.

2.5 STABILITY OF THE SAMPLES

The stability of Bitumen stored in the metal cans was checked. The material has been found sufficiently stable for the period of the proficiency test.

2.6 ANALYZES

The participants were requested to determine: Density at 25 °C, Dynamic Viscosity at 60 °C, Flash Point C.O.C., Fraass Breaking Point, Kinematic Viscosity at 135 °C, Penetration at 25 °C, Penetration Index, RTFOT at 163 °C (Change of Mass, Retained Penetration, Viscosity Ratio and Increase in Softening Point), Softening Point (Ring and Ball), Solubility in Xylene and Ductility.

It was explicitly requested to treat the sample as if it was a routine sample and to report the test results using the indicated units on the report form and not to round the test results, but report as much significant figures as possible. It was also requested not to report 'less than' test results, which are above the detection limit, because such test results cannot be used for meaningful statistical evaluations.

To get comparable test results a detailed report form and a letter of instructions are prepared. On the report form the reporting units are given as well as the reference test methods (when applicable) that will be used during the evaluation. The detailed report form and the letter of instructions are both made available on the data entry portal www.kpmd.co.uk/sgs-iis/. The participating laboratories are also requested to confirm the sample receipt on this data entry portal. The letter of instructions can also be downloaded from the iis website www.iisnl.com.

3 RESULTS

During five weeks after sample dispatch, the test results of the individual laboratories were gathered via the data entry portal www.kpmd.co.uk/sgs-iis/. The reported test results are tabulated per determination in appendix 1 of this report. The laboratories are presented by their code numbers.

Directly after the deadline a reminder was sent to those laboratories that had not reported test results at that moment. Shortly after the deadline, the available test results were screened for suspect data. A test result was called suspect in case the Huber Elimination Rule (a robust outlier test) found it to be an outlier. The laboratories that produced these suspect data were asked to check the reported test results (no reanalyzes). Additional or corrected test results are used for data analysis and the original test results are placed under 'Remarks' in the result tables in appendix 1. Test results that came in after the deadline were not taken into account in this screening for suspect data and thus these participants were not requested for checks.

3.1 STATISTICS

The protocol followed in the organization of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of June 2018 (iis-protocol, version 3.5).

For the statistical evaluation the *unrounded* (when available) figures were used instead of the rounded test results. Test results reported as '<...' or '>...' were not used in the statistical evaluation.

First, the normality of the distribution of the various data sets per determination was checked by means of the Lilliefors-test, a variant of the Kolmogorov-Smirnov test and by the calculation of skewness and kurtosis. Evaluation of the three normality indicators in combination with the visual evaluation of the graphic Kernel density plot, lead to judgement of the normality being either 'unknown', 'OK', 'suspect' or 'not OK'. After removal of outliers, this check was repeated. If a data set does not have a normal distribution, the (results of the) statistical evaluation should be used with due care. The assigned value is determined by consensus based on the test results of the group of participants after rejection of the statistical outliers and/or suspect data.

According to ISO13528 all (original received or corrected) results per determination were submitted to outlier tests. In the iis procedure for proficiency tests, outliers are detected prior to calculation of the mean, standard deviation and reproducibility. For small data sets, Dixon (up to 20 test results) or Grubbs (up to 40 test results) outlier tests can be used. For larger data sets (above 20 test results) Rosner's outlier test can be used. Outliers are marked by D(0.01) for the Dixon's test, by G(0.01) or DG(0.01) for the Grubbs' test and by R(0.01) for the Rosner's test. Stragglers are marked by D(0.05) for the Dixon's test, and by R(0.05) for the Rosner's test. Both outliers and stragglers were not included in the calculations of averages and standard deviations.

For each assigned value the uncertainty was determined in accordance with ISO13528. Subsequently the calculated uncertainty was evaluated against the respective requirement based on the target reproducibility in accordance with ISO13528. In this PT, the criterion of ISO13528, paragraph 9.2.1. was met for all evaluated tests, therefore, the uncertainty of all assigned values may be negligible and need not be included in the PT report.

Finally, the reproducibilities were calculated from the standard deviations by multiplying them with a factor of 2.8.

3.2 GRAPHICS

In order to visualize the data against the reproducibilities from literature, Gauss plots were made, using the sorted data for one determination (see appendix 1). On the Y-axis the reported test results are plotted. The corresponding laboratory numbers are on the X-axis. The straight horizontal line presents the consensus value (a trimmed mean). The four striped lines, parallel to the consensus value line, are the +3s, +2s, -2s and -3s target reproducibility limits of the selected reference test method. Outliers and other data, which were excluded from the calculations, are represented as a cross. Accepted data are represented as a triangle.

Furthermore, Kernel Density Graphs were made. This is a method for producing a smooth density approximation to a set of data that avoids some problems associated with histograms. Also, a normal Gauss curve (dotted line) was projected over the Kernel Density Graph (smooth line) for reference. The Gauss curve is calculated from the consensus value and the corresponding standard deviation.

3.3 Z-SCORES

To evaluate the performance of the participating laboratories the z-scores were calculated. As it was decided to evaluate the performance of the participants in this proficiency test (PT) against the literature requirements (derived from e.g. ISO or ASTM test methods), the z-scores were calculated using a target standard deviation. This results in an evaluation independent of the variation in this interlaboratory study. The target standard deviation was calculated from the literature reproducibility by division with 2.8. In case no literature reproducibility was available, other target values were used, like Horwitz or an estimated reproducibility based on former iis proficiency tests.

When a laboratory did use a test method with a reproducibility that is significantly different from the reproducibility of the reference test method used in this report, it is strongly advised to recalculate the z-score, while using the reproducibility of the actual test method used, this in order to evaluate whether the reported test result is fit-for-use.

The z-scores were calculated according to:

z(target) = (test result - average of PT) / target standard deviation

The z(target) scores are listed in the test result tables in appendix 1.

Absolute values for z<2 are very common and absolute values for z>3 are very rare. The usual interpretation of z-scores is as follows:

|z| < 1 good 1 < |z| < 2 satisfactory 2 < |z| < 3 questionable 3 < |z| unsatisfactory

4 EVALUATION

In this proficiency test some problems were encountered with the dispatch of the samples. Six participants reported test results after the final reporting date and two other participants did not report any test results. Not all participants were able to report all tests requested. Finally, 45 participants reported in total 318 numerical test results. Observed were 15 outlying test results, which is 4.7%. In proficiency studies outlier percentages of 3% - 7.5% are quite normal.

All data sets proved to have a normal Gaussian distribution.

4.1 EVALUATION PER TEST

In this section the reported test results are discussed per test. The test methods which were used by the various laboratories were taken into account for explaining the observed differences when possible and applicable. These test methods are also in the tables together with the original data in appendix 1. The abbreviations, used in these tables, are explained in appendix 3.

In the iis PT reports ASTM test methods are referred to with a number (e.g. D36) and an added designation for the year that the test method was adopted or revised (e.g. D36:14). When a method has been reapproved an "R" will be added and the year of approval (e.g. D36:14R20).

<u>Density at 25 °C</u>: This determination was not problematic. Two statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of EN15326:07+A1:09.

<u>Dynamic Viscosity at 60 °C</u>: This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of EN12596:14.

- <u>Flash Point C.O.C.</u>: This determination was problematic. Two statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is not in agreement with the requirements of ISO2592:17 or ASTM D92:18.
- <u>Fraass Breaking Point</u>: This determination was problematic. No statistical outliers were observed. The calculated reproducibility is not in agreement with the requirements of EN12593:15.

<u>Kinematic Viscosity at 135 °C</u>: This determination was problematic. No statistical outliers were observed. The calculated reproducibility is not in agreement with the requirements of EN12595:14 or ASTM D2170:18.

Penetration at 25 °C: This determination may be problematic depending on the test method used. No statistical outliers were observed. The calculated reproducibility is not in agreement with the requirements of EN1426:15 but is in full agreement with the requirements of ASTM D5:20. When the test results of test method EN1426 and ASTM D5 are evaluated separately, the reproducibility for the EN1426 test results is still not in agreement but it is in agreement for ASTM D5 test results. Different factors could cause this large variation, such as preparation, temperature and needle. During the measurement, the temperature should be kept at 25 °C, by immersing the sample in enough water of this temperature. For measurements outside of the waterbath, a transfer dish of 350 ml should be used. Deviations from this temperature will have influence on the penetration. Another factor is the tip of the needle used. This tip should keep the same dimensions/surface through out testing in time. In practise, it will get abrasion and wear and should be replaced regularly.

- <u>Penetration Index</u>: This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of EN12591:09.
- <u>RTFOT at 163 °C Change of Mass</u>: The determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of EN12607-1:14.

<u>RTFOT at 163 °C - Retained Penetration</u>: The determination was not problematic. Two statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of EN12607-1:14.

<u>RTFOT at 163 °C - Viscosity Ratio</u>: The determination was problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is not in agreement with the requirements of EN12607-1:14.

- <u>RTFOT at 163 °C on Increase in Softening Point</u>: The determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of EN12607-1:14.
- <u>Softening Point (Ring and Ball)</u>: This determination was not problematic. Five statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of EN1427:15 and ASTM D36:14R20.
- <u>Solubility in Xylene</u>: This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of EN12595:14.
- <u>Ductility</u>: This determination was not problematic. All reporting participants, except one, agreed on a test result >100 cm.

4.2 **PERFORMANCE EVALUATION FOR THE GROUP OF LABORATORIES**

A comparison has been made between the reproducibility as declared by the reference test method and the reproducibility as found for the group of participating laboratories. The number of significant test results, the average, the calculated reproducibility (2.8 * standard deviation) and the target reproducibility derived from reference methods are presented in the next table.

| Parameter | unit | n | average | 2.8 * sd | R(lit) |
|---------------------------------|-------------------|----|---------|----------|--------|
| Density at 25 °C | kg/m ³ | 28 | 1044.2 | 5.4 | 5 |
| Dynamic Viscosity at 60 °C | Pa.s | 12 | 709 | 73 | 71 |
| Flash Point C.O.C. | °C | 23 | 315 | 28 | 18 |
| Fraass Breaking Point | °C | 19 | -11.3 | 7.7 | 6 |
| Kinematic Viscosity at 135 °C | mm²/s | 17 | 747.6 | 79.8 | 67.3 |
| Penetration at 25 °C | 0.1 mm | 45 | 44.3 | 5.5 | 3 |
| Penetration Index | | 20 | -0.49 | 0.35 | 0.5 |
| RTFOT - Change of Mass | % | 26 | -0.15 | 0.20 | 0.2 |
| RTFOT - Retained Penetration | % | 24 | 65.2 | 9.7 | 10 |
| RTFOT - Viscosity Ratio | | 9 | 3.2 | 0.8 | 0.6 |
| RTFOT - Increase in Soft. Point | °C | 25 | 7.1 | 3.0 | 4 |
| Softening Point (Ring & Ball) | °C | 39 | 54.1 | 1.6 | 2 |

| Parameter | unit | n | average | 2.8 * sd | R(lit) |
|----------------------|------|----|---------|----------|--------|
| Solubility in Xylene | %M/M | 16 | 99.87 | 0.16 | 0.15 |
| Ductility | cm | 10 | >100 | n.a. | n.a. |

 Table 3: reproducibilities of tests on sample #22240

Without further statistical calculations it can be concluded that for many tests there is a good compliance of the group of participants with the reference test methods. The problematic tests have been discussed in paragraph 4.1.

4.3 COMPARISON OF THE PROFICIENCY TEST OF NOVEMBER 2022 WITH PREVIOUS PTS

| | November 2022 | December 2021 | December 2020 | December 2019 | December 2018 |
|------------------------------------|------------------|------------------|------------------|------------------|------------------|
| Number of reporting laboratories | 45 | 51 | 50 | 45 | 37 |
| Number of test results | 318 | 348 | 315 | 310 | 511 |
| Number of statistical outliers | 15 | 11 | 14 | 11 | 15 |
| Percentage of statistical outliers | 4.7% | 3.2% | 4.4% | 3.5% | 2.9% |

Table 4: comparison with previous proficiency tests

In proficiency tests, outlier percentages of 3% - 7.5% are quite normal.

The performance of the determinations of the proficiency tests was compared to the requirements of the reference test methods. The conclusions are given in the following table.

| Parameter | November 2022 | December 2021 | December 2020 | December 2019 | Dece 20 | mber 18 |
|-------------------------------------|------------------|------------------|------------------|------------------|------------|------------|
| Paving Grade | 35/50 | 70/100 | 35/50 | 70/100 | 70/100 | 35/50 |
| Density at 25 °C | +/- | +/- | - | - | - | |
| Dynamic Viscosity at 60 °C | +/- | - | | - | + | - |
| Flash Point C.O.C. | - | | () | - | - | |
| Fraass Breaking Point | - | - | - | +/- | + | +/- |
| Kinematic Viscosity at 135 °C | - | - | | - | - | - |
| Penetration at 25 °C | - | - | | - | - | |
| Penetration Index | + | +/- | +/- | - | + | + |
| RTFOT - Change of Mass | +/- | - | ++ | | () | +/- |
| RTFOT - Retained Penetration | +/- | +/- | - | +/- | - | - |
| RTFOT - Viscosity Ratio | - | +/- | n.e. | () | + | +/- |
| RTFOT - Increase in Soft. Point | + | + | +/- | - | +/- | +/- |
| Softening Point (Ring and Ball) | + | +/- | - | +/- | + | + |
| Solubility in Xylene | +/- | () | () | () | +/- | + |

Table 5: comparison determinations to the reference test methods

For results between brackets no z-scores are calculated

In the table above the following performance categories were used:

- ++ : group performed much better than the reference test method
- + : group performed better than the reference test method
- +/- : group performance equals the reference test method
- : group performed worse than the reference test method
- -- : group performed much worse than the reference test method
- n.e. : not evaluated

APPENDIX 1

Determination of Density at 25 °C on sample #22240; results in kg/m³

| lab | method | value | mark | z(targ) | remarks |
|------|----------------------------|----------|---------|---------|--|
| 154 | D70 | 1044 | С | -0.10 | first reported: 1.044 kg/m ³ |
| 225 | D70 | 1046 | | 1.02 | 1 0 |
| 328 | EN15326 | 1045 | С | 0.46 | first reported: 1.045 kg/m ³ |
| 333 | | | | | |
| 335 | EN15326 | 1047 | С | 1.58 | first reported: 1.047 kg/m ³ |
| 342 | D70 | 1042 | | -1.22 | |
| 357 | | | | | |
| 360 | EN15326 | 1046.40 | | 1.24 | |
| 365 | | | | | |
| 396 | EN15326 | 1046.2 | | 1.13 | |
| 398 | | | | | |
| 399 | D70 | 1046.1 | | 1.07 | |
| 444 | | | | | |
| 447 | D70 | 1043 | | -0.66 | |
| 604 | D70 | 1042.8 | С | -0.78 | first reported: 1049.2 |
| 657 | D70 | 1043 | | -0.66 | |
| 736 | EN15326 | 1046.7 | | 1.41 | |
| 781 | EN15326 | 1042.5 | | -0.94 | |
| 865 | | | | | |
| 904 | D70 | 1053.3 | R(0.01) | 5.10 | |
| 1011 | D70 | 1046 | С | 1.02 | first reported: 1.046 kg/m ³ |
| 1016 | EN15326 | 1047.6 | С | 1.91 | first reported: 1.0476 kg/m ³ |
| 1026 | EN15326 | 1043 | | -0.66 | |
| 1040 | ISU3838 | 1044.2 | 0 | 0.01 | First way arts of A 0405 law (m-3 |
| 1108 | EN15326 | 1042.5 | C | -0.94 | first reported: 1.0425 kg/m° |
| 1135 | EN 15320 | 1044 | | -0.10 | |
| 1402 | EN 13320 | 1042.3 | | -1.00 | |
| 1402 | DIN51757 | 1042.0 | | -0.69 | |
| 1631 | DINSTIST | 1042.0 | | -0.09 | |
| 1724 | | | | | |
| 1730 | EN15326 | 1042.0 | C | -1 22 | first reported: 1.0420 kg/m ³ |
| 1833 | 21110020 | | 0 | | |
| 1849 | | | | | |
| 1852 | | | | | |
| 1857 | D70 | 1045.3 | | 0.62 | |
| 1881 | EN15326 | 1043.1 | | -0.61 | |
| 1944 | EN15326 | 1047.2 | | 1.69 | |
| 1990 | | | | | |
| 6037 | | | | | |
| 6076 | | | | | |
| 6228 | | | | | |
| 6229 | EN15326 | 1041 | | -1.78 | |
| 6364 | D70 | 1043.1 | | -0.61 | |
| 6404 | ISO12185 | 1032 | R(0.01) | -6.82 | |
| 6419 | | | | | |
| 6474 | | | | | |
| | | | | | |
| | normality | OK | | | |
| | | 20 | | | |
| | | Z | | | |
| | nicali (II) st dev. (n) | 1044.100 | | | |
| | R(calc.) | 5 352 | | | |
| | st dev (FN15326·07+Δ1·00) | 1 786 | | | |
| | R(FN15326: 07+A1:09) | 5 | | | |
| | | 2 | | | |



method

lab

Determination of Dynamic Viscosity at 60 °C on sample #22240; results in Pa.s

z(targ)

remarks

mark

value

| 365 396 398 399 444 447 604 657 736 781 865 904 | EN12596 D2171 EN12596 EN12596 | 608 704 696.8 675.4 | G(0.05) | -4.01 -0.22 -0.50 -1.35 | | | | |
|--|---|--|---------|--|---|-----|---|--|
| 1011 1016 1026 1040 1108 1135 | EN12596 | 703.36 767 679 | | -0.24 2.27 -1.20 | | | | |
| 1378 1402 1613 1631 1724 | EN12596 | 730 | | 0.81 | | | | |
| 1730 1833 1849 1852 1857 1881 1944 1990 6037 | EN12596 D2171 | 710.4 705.9 | | 0.04 -0.14 | | | | |
| 6076 6228 6229 6364 | EN12596 | 720 | | 0.77 | | | | |
| 6404 6419 6474 | | | | | | | | |
| 6404 6419 6474 | normality n outliers mean (n) st.dev. (n) R(calc.) st.dev.(EN12596:14) R(EN12596:14) | 729 OK 12 1 709.49 25.911 72.55 25.339 70.95 | | | | | | |
| | normality n outliers mean (n) st.dev. (n) R(calc.) st.dev.(EN12596:14) R(EN12596:14) | 729 OK 12 1 709.49 25.911 72.55 25.339 70.95 | | | | | Δ | 0.018 0.016 - Kernel Density 0.014 - |
| | normality n outliers mean (n) st.dev. (n) R(calc.) st.dev.(EN12596:14) R(EN12596:14) | A A | Δ | | Δ | Δ Δ | Δ | 0.018 0.016 0.014 0.012 0.011 0.012 0.01 0.008 0.008 0.006 0.004 |

Determination of Flash Point C.O.C. on sample #22240; results in °C

| lah | method | value | mark | z(tara) | romarks | | |
|------------|---------------------|--------|-----------|---------|----------------------|--------|----------------|
| 154 | D92 automated | 320 | IIIdi K | 0.80 | Temarka | | |
| 225 | D92 manual | 314.0 | | -0.13 | | | |
| 328 | | | | | | | |
| 333 | | | | | | | |
| 335 | | | | | | | |
| 342 | ISO2592 automated | 322 | | 1.11 | | | |
| 357 | ISO2592 automated | 314 | | -0.13 | | | |
| 300 | ISO2592 automated | 292.0 | | -3.50 | | | |
| 305 | 1502592 | 320 | | 0.80 | | | |
| 398 | 1002002 | 520 | | | | | |
| 399 | | | | | | | |
| 444 | | | | | | | |
| 447 | | | | | | | |
| 604 | D92 manual | 308 | | -1.07 | | | |
| 657 | D92 manual | 318 | | 0.49 | | | |
| 736 | ISO2592 automated | 328 | D(0.01) | 2.04 | | | |
| 781 | 1502592 | 232.5 | R(0.01) | -12.81 | | | |
| 903 904 | 1502592 | 323 | | 1 27 | | | |
| 1011 | ISO2592 automated | >280 | | | | | |
| 1016 | ISO2592 automated | 324 | | 1.42 | | | |
| 1026 | ISO2592 manual | 314 | | -0.13 | | | |
| 1040 | | | | | | | |
| 1108 | | | | | | | |
| 1135 | ISO2592 automated | 307.0 | | -1.22 | | | |
| 1378 | ISO2592 automated | 335 | | 3.13 | | | |
| 1402 | ISO2592 manual | >300 | C | 2.21 | first reported: 250 | | |
| 1631 | ISO2592 automated | 318 | C | -2.31 | liist reported. 250 | | |
| 1724 | D92 manual | 308 | | -1 07 | | | |
| 1730 | 202 | | | | | | |
| 1833 | ISO2592 automated | 318 | | 0.49 | | | |
| 1849 | ISO2592 automated | 315.7 | | 0.13 | | | |
| 1852 | | | | | | | |
| 1857 | D92 manual | 314 | | -0.13 | | | |
| 1881 | ICO2E02 manual | | | | | | |
| 1944 | 1502592 manual | 312 | | -0.44 | | | |
| 6037 | | | | | | | |
| 6076 | | | | | | | |
| 6228 | | | | | | | |
| 6229 | ISO2592 automated | 322 | | 1.11 | | | |
| 6364 | D92 automated | 222 | C,R(0.01) | -14.44 | first reported:238.0 | | |
| 6404 | ISO2592 manual | 295 | | -3.09 | | | |
| 6419 | | | | | | | |
| 0474 | | | | | | | |
| | normality | OK | | | | | |
| | n | 23 | | | | | |
| | outliers | 2 | | | | | |
| | mean (n) | 314.86 | | | | | |
| | st.dev. (n) | 10.041 | | | | | |
| | R(calc.) | 28.11 | | | | | |
| | st.dev.(ISO2592:17) | 6.429 | | | | | |
| compar | R(ISO2592:17) | 18 | | | | | |
| compai | R(D92.18) | 18 | | | | | |
| | 1((002.10) | 10 | | | | | |
| 240 | | | | | | 0.045 |] |
| 340 T | | | | | Δ | 0.043 | Kernel Density |
| 330 - | | | | | | 0.04 - | |
| | | | | | | 0.035 | |
| 320 + | | | Δ | ۵ ۵ | Δ | 0.03 - | |
| | | Δ Λ | A A " | | | 0.025 | |



Determination of Fraass Breaking Point on sample #22240; results in °C

| lab | method | value | mark | z(targ) | remarks | | |
|----------------|---------------------|--------|------|---------|---------|--------|----------------|
| 154 | | | | | | | |
| 225 | | | | | | | |
| 328 | | | | | | | |
| 333 | | | | | | | |
| 335 | | | | | | | |
| 342 | | | | | | | |
| 357 | EN12593 automated | -11 | | 0.14 | | | |
| 360 | EN12593 automated | -11.2 | | 0.05 | | | |
| 365 | | | | | | | |
| 396 | EN12593 | -7 | | 2.01 | | | |
| 398 | | | | | | | |
| 399 | | | | | | | |
| 444 | | | | | | | |
| 604 | | | | | | | |
| 657 | | | | | | | |
| 736 | EN12593 automated | -14 | | -1 26 | | | |
| 781 | EN12593 automated | -11.5 | | -0.09 | | | |
| 865 | | | | | | | |
| 904 | EN12593 manual | -9 | | 1.08 | | | |
| 1011 | EN12593 automated | -13 | | -0.79 | | | |
| 1016 | EN12593 automated | -11 | | 0.14 | | | |
| 1026 | | -14 | | -1.26 | | | |
| 1040 | | | | | | | |
| 1108 | | | | | | | |
| 1135 | EN12593 automated | -15 | | -1.72 | | | |
| 1378 | | | | | | | |
| 1402 | EN12593 manual | -6 | | 2.48 | | | |
| 1613 | | | | | | | |
| 1031 | | | | | | | |
| 1724 | EN12503 automated | 10.5 | | 0.38 | | | |
| 1833 | LIN 12595 automateu | -10.5 | | 0.50 | | | |
| 1849 | | | | | | | |
| 1852 | EN12593 automated | -13 | | -0 79 | | | |
| 1857 | EN12593 automated | -11.7 | | -0.18 | | | |
| 1881 | | | | | | | |
| 1944 | EN12593 automated | -9 | | 1.08 | | | |
| 1990 | | | | | | | |
| 6037 | | | | | | | |
| 6076 | EN12593 automated | -10 | | 0.61 | | | |
| 6228 | EN12593 automated | -14 | | -1.26 | | | |
| 6229 | EN12593 automated | -8 | | 1.54 | | | |
| 6364 | | | | | | | |
| 6404 | EN12593 automated | -16 | | -2.19 | | | |
| 6419 | | | | | | | |
| 0474 | | | | | | | |
| | normality | OK | | | | | |
| | n | 19 | | | | | |
| | outliers | 0 | | | | | |
| | mean (n) | -11.31 | | | | | |
| | st.dev. (n) | 2.730 | | | | | |
| | R(calc.) | 7.65 | | | | | |
| | st.dev.(EN12593:15) | 2.14 | | | | | |
| | R(EN12593:15) | 6 | | | | | |
| | | | | | | | |
| 0 _T | | | | | | 0.16 - | |
| -2 | | | | | | 0.14 | Kernel Density |



method

lab

Determination of Kinematic Viscosity at 135 °C on sample #22240; results in mm²/s

z(targ)

remarks

mark

value

| 154 225 328 333 335 342 357 360 365 396 398 399 444 447 604 657 736 781 865 904 | EN12595 EN12595 D2170 EN12595 EN12595 EN12595 | 739 717 725 725 742 711.1 754.9 785 745 | С | -0.30 -1.27 -0.94 -0.23 -1.52 0.31 1.56 | first reported: 597 | | | |
|--|--|---|-----|---|----------------------------|------|---|----------------|
| 1011 1016 1026 1040 1108 | EN 12395 EN 12595 EN 12595 | 745 734.7 706 | | -0.11 -0.54 -1.73 | | | | |
| 1135 1378 1402 1613 1631 1724 | EN12595 EN12595 D2170 | 745 766.6 792 | | -0.11 0.79 1.85 | | | | |
| 1730 1833 1849 1852 | EN12595 | 753.7 | | 0.26 | | | | |
| 1857 1881 1944 1990 6037 6076 6228 6229 6364 6429 6464 6419 6474 | D445 EN12595 | /54.7 726.9 810 | | 0.30 -0.86 2.60 | | | | |
| compar | normality n outliers mean (n) st.dev. (n) R(calc.) st.dev.(EN12595:14) R(EN12595:14) e | OK 17 0 747.56 28.493 79.78 24.029 67.28 | | | | | | |
| ⁸³⁰ [| R(D2170:18) | 65.79 | | | | | 0.016 | Kernel Density |
| 810 + 730 750 730 710 690 | ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ | Δ Δ | Δ | <u>ه م</u> | ۵ ۵ | | 0.014 - 0.012 - 0.01 - 0.008 - 0.006 - 0.004 - | Kernei Density |
| 650 | 736 357 320 6229 6229 | 154 657 | 101 | 1857 | 781 1402 804 1613 | 6404 | 0.002 | 700 800 900 |

Determination of Penetration at 25 °C on sample #22240; results in 0.1 mm

| lab | method | value | mark | z(targ) | remarks | |
|---------------|--|---------------------------------|---------------------------------|--------------------------|---|----------------|
| 154 | D5 manual | 45 | | 0.69 | | |
| 225 | D5 manual | 44.0 | | -0.25 | | |
| 328 | EN1426 manual | 46 | | 1.62 | | |
| 333 | EN1426 manual | 44 | | -0.25 | | |
| 335 | EN1426 automated | 40 | | 1.62 | | |
| 342 | EN1426 manual | 44 | | -0.25 | | |
| 360 | EN1426 automated | 47 | | 2.00 | | |
| 365 | EN1420 automated | 40.7 | | -3.33 | | |
| 396 | EN1420 | 45.40 | | 0.69 | | |
| 398 | FN1426 manual | 45 | | 0.69 | | |
| 399 | EN1426 manual | 45 | | 0.69 | | |
| 444 | EN1426 manual | 40.8 | | -3.23 | | |
| 447 | EN1426 automated | 44 | | -0.25 | | |
| 604 | D5 manual | 42 | | -2.11 | | |
| 657 | D5 manual | 44 | | -0.25 | | |
| 736 | EN1426 automated | 47 | | 2.55 | | |
| 781 | EN1426 automated | 42 | | -2.11 | | |
| 865 | | | | | | |
| 904 | EN1426 | 44 | | -0.25 | | |
| 1011 | EN1426 automated | 44 | | -0.25 | | |
| 1016 | EN1426 automated | 40 | | 1.62 | | |
| 1020 | EN1426 outomated | 40 | | 1.02 | | |
| 1040 | EN1420 automated | 45.0 | | 1.62 | | |
| 1135 | EN1420 automated | 40 45 | | 0.60 | | |
| 1378 | EN1426 automated | 43 | | 3 40 | | |
| 1402 | EN1426 manual | 43 | | -1 18 | | |
| 1613 | D5 automated | 40.0 | | -3.98 | | |
| 1631 | EN1426 automated | 44 | | -0.25 | | |
| 1724 | D5 manual | 44 | | -0.25 | | |
| 1730 | EN1426 automated | 45.8 | | 1.43 | | |
| 1833 | EN1426 automated | 43 | | -1.18 | | |
| 1849 | EN1426 automated | 43.4 | | -0.81 | | |
| 1852 | EN1426 automated | 42 | | -2.11 | | |
| 1857 | EN1426 manual | 46.2 | | 1.81 | | |
| 1881 | EN1426 automated | 45.0 | | 0.69 | | |
| 1944 | EN1426 automated | 41 | | -3.05 | | |
| 1990 | D5 manual | 41 | | -3.05 | | |
| 6037 | EN1426 manual | 41.4 | | -2.67 | | |
| 6076 | EN1426 automated | 47 | | 2.55 | | |
| 6228 | EN1426 automated | 47.25 | | 2.79 | | |
| 6229 | EN1426 automated | 45 | 0 | 0.69 | finat na na sta da 07 | |
| 6404 | D5 manual | 42 | C | -2.11 | first reported: 37 | |
| 6404 | EN1420 manual | 44 | | -0.25 | | |
| 6474 | EN 1420 Mariuar | 45.9 | | 1.55 | | |
| 0474 | | | | | | |
| | | | | | Only FN1426 | Only D5 |
| | normality | OK | | | OK | OK |
| | n | 45 | | | 36 | 9 |
| | outliers | 0 | | | 0 | 0 |
| | mean (n) | 44.265 | | | 44.553 | 43.111 |
| | st.dev. (n) | 1.9799 | | | 1.9020 | 1.9650 |
| | R(calc.) | 5.544 | | | 5.326 | 5.502 |
| | st.dev.(EN1426:15) | 1.0714 | | | 1.0714 | |
| | R(EN1426:15) | 3 | | | 3 | |
| compar | | 7 075 | | | | 7.075 |
| | R(D5:20) | 1.075 | | | | 7.075 |
| | | | | | | 0.05 |
| ⁴⁹ | | | | | | 0.25 |
| 48 + | | | | | ^ | Kernel Density |
| 47 + | | | | | | |
| 46 + | | | | | A A A A A A A A A A A A A A A A A A A | |
| 45 - | | | ΔΔΔ | ΔΔΔΔ | | 0.15 - |
| 44 - | | | ΔΔ | | | |
| 43 + | ۵ ۵ | | | | | 0.1 |
| 42 | Δ Δ Δ Δ | | | | | |
| 41 <u>A</u> A | <u>λ</u> λ - | | | | | 0.05 - // |
| 40 + 🛆 | | | | | | |
| 30 T | 944 990 804 804 952 933 933 949 147 147 | 333 011 225 304 331 | 724 404 154 398 398 | 386 135 381 229 | 365 730 016 016 335 736 736 736 736 736 736 736 736 736 736 | |
| ₩ ~ ~ 4 | 5 5 9 4 8 4 4 4 9 4 9 | | 4 0 1 1 1 1 | | | |
| | | | | | | |

Determination of Penetration Index on sample #22240;

| lab | method | value | mark | z(targ) | remarks | | | |
|----------------|----------------------|----------|----------|------------|---------|-------|----------|----------------|
| 154 | EN12591 | -0.5 | | -0.07 | | | | |
| 225 | | | | | | | | |
| 328 | | | | | | | | |
| 333 | | | | | | | | |
| 335 | | | | | | | | |
| 342 | EN12591 | -0.6 | | -0.63 | | | | |
| 360 | EN12391 | -0.4 | | 0.49 | | | | |
| 365 | | | | | | | | |
| 396 | EN12591 | -0.42 | | 0.38 | | | | |
| 398 | | | | | | | | |
| 399 | | | | | | | | |
| 444 | | | | | | | | |
| 447 | | | | | | | | |
| 657 | Calculation | -0.3 | | 1.05 | | | | |
| 736 | EN12591 | -0.49 | | -0.01 | | | | |
| 781 | EN12591 | -0.5 | | -0.07 | | | | |
| 865 | | | | | | | | |
| 904 | EN12591 | 0.3 | R(0.01) | 4.41 | | | | |
| 1011 | EN12591 | -0.5 | | -0.07 | | | | |
| 1016 | EN12591 | -0.49 | | -0.01 | | | | |
| 1026 | EN12591 | -0.2 | | 1.61 | | | | |
| 1040 | EN 12091 EN 12501 | -0.7 | | -1.19 | | | | |
| 1135 | EN12591 | -0.515 | | -0.13 | | | | |
| 1378 | EN12591 | -0.39 | | 0.55 | | | | |
| 1402 | | -0.6 | | -0.63 | | | | |
| 1613 | | | | | | | | |
| 1631 | | | | | | | | |
| 1724 | | | | | | | | |
| 1/30 | | | | | | | | |
| 1840 | | | | | | | | |
| 1852 | EN12591 | -0 47 | | 0 10 | | | | |
| 1857 | EN12591 | -0.45 | | 0.21 | | | | |
| 1881 | | | | | | | | |
| 1944 | EN12591 | -0.570 | | -0.46 | | | | |
| 1990 | | | | | | | | |
| 6037 | | | | | | | | |
| 6228 | | | | | | | | |
| 6229 | EN12591 | -0.7 | | _1 19 | | | | |
| 6364 | 21112001 | | | | | | | |
| 6404 | EN12591 | -0.37 | | 0.66 | | | | |
| 6419 | | | | | | | | |
| 6474 | | | | | | | | |
| | | | | | | | | |
| | normality | 0K 20 | | | | | | |
| | outliers | 1 | | | | | | |
| | mean (n) | -0.488 | | | | | | |
| | st.dev. (n) | 0.1238 | | | | | | |
| | R(calc.) | 0.347 | | | | | | |
| | st.dev.(EN12591:09) | 0.1786 | | | | | | |
| | R(EN12591:09) | 0.5 | | | | | | |
| | | | | | | | | 1 |
| ^{0.5} | | | | | | 3.5 | <u>^</u> | Kernel Density |
| 0.3 | | | | | x | 3 - | \wedge | Remer Density |
| 0.1 | | | | | | 2.5 | // // | |
| -0.1 - | | | | | | | | |
| -0.3 - | | | | | Δ | 2 | | |
| -0.5 | | A | <u> </u> | <u>م م</u> | Δ Δ | 1.5 - | | |
| -0.7 | | | | | | 1 - | | |

 .n q

0.5

0.5

0 ↓ -1

-0.5

Determination of RTFOT at 163 $^\circ\text{C},$ Change of Mass on sample #22240; results in %

| lab | method | value | mark | z(targ) | remarks |
|------------|---|---|--------------|-----------------|--|
| 154 | D2872 | -0.217 | | -0.87 | |
| 225 | | | | | |
| 328 | | | | | |
| 335 335 | | | | | |
| 342 | | | | | |
| 357 | EN12607-1 | -0.13 | | 0.35 | |
| 360 | EN12607-1 | -0.194 | | -0.55 | |
| 365 | | | | | |
| 390 | EN 12007-1 | -0.15 | | 0.07 | |
| 399 | | | | | |
| 444 | | | | | |
| 447 | | | | | |
| 604 657 | 02872 | | | 0.01 | |
| 736 | EN12607-1 | -0.09 | | 1 76 | |
| 781 | EN12607-1 | -0.121 | | 0.47 | |
| 865 | | | | | |
| 904 | EN12607-1 | -0.16 | | -0.07 | |
| 1011 | EN12607-1 | -0.25 | | -1.33 | |
| 1010 | LN12007-1 | -0.28 | | 1.75 | |
| 1040 | | | | | |
| 1108 | EN12607-1 | -0.193 | | -0.53 | |
| 1135 | EN12607-1 | -0.12 | 0 | 0.49 | First serviced 0.440 |
| 1378 | EN12607-1 EN12607-1 | -0.140 -0.16 | C | 0.21 | first reported: 0.140 |
| 1613 | D2872 | -0.10 | | 0.77 | |
| 1631 | EN12607-1 | -0.21 | | -0.77 | |
| 1724 | | -0.19 | | -0.49 | |
| 1730 | EN12607-1 | -0.217 | | -0.87 | |
| 1849 | EN12607-1 | -0.17 | | -0.21 | |
| 1852 | | | | | |
| 1857 | EN12607-1 | -0.205 | | -0.70 | |
| 1881 | | | 0 | | Frank and a second seco |
| 1944 | EN12007-1 | -0.089 | C | 0.92 | lirst reported: -0.389 |
| 6037 | | | | | |
| 6076 | | | | | |
| 6228 | | | | | |
| 6229 | EN12607-1 | -0.23 | <u> </u> | -1.05 | first reported: 0.0100 |
| 6404 | EN12607-1 | -0.15 | C | 2.45 | list reported. 0.0196 |
| 6419 | | | | | |
| 6474 | | | | | |
| | | | | | |
| | normality | 0K 26 | | | |
| | outliers | 0 | | | |
| | mean (n) | -0.1548 | | | |
| | st.dev. (n) | 0.07189 | | | |
| | R(calc.) | 0.2013 | | | |
| | SI.UEV.(EINT2007-1:14) R(EN12607-1:14) | 0.07 143 | | | |
| | | 0.2 | | | |
| 0.1 T | | | | | 6 |
| — — | | | | | Kernel Density |
| 0 † — | | | | | " 5 · // \\ |
| -0.1 | | | | | |
| - | | <u>ــــــــــــــــــــــــــــــــــــ</u> | <u>Δ Δ Δ</u> | ΔΔ ⁴ | · · · · · · · · · · · · · · · · · · · |
| -0.2 | | ΔΔ | | | |
| -0.3 | - | | | | |

 -0.4

-0.5

 0.2

1 -0 -0.6

-0.4

-0.2

Determination of RTFOT at 163 °C, Retained Penetration on sample #22240; results in %

| lab | method | value | mark | z(targ) | remarks |
|--------------|---|--------------|-----------|---------|-----------------------|
| 154 | D2872 | 68.9 | | 1.03 | |
| 225 | | | | | |
| 328 | | | | | |
| 333 | | | | | |
| 335 | | | | | |
| 342 | EN12607 1 | | | | |
| 357 | EN12007-1 | 03.0 | | -0.40 | |
| 365 | EN12007-1 | 70.0 | | 1.50 | |
| 396 | EN12607-1 | 68.89 | | 1.03 | |
| 398 | | | | | |
| 399 | | | | | |
| 444 | | | | | |
| 447 | | | | | |
| 604 | D0070 | | | | |
| 057 726 | D2872 EN12607 1 | 68 65 06 | | 0.78 | |
| 781 | EN12007-1 | 64 29 | | -0.21 | |
| 865 | EN12007-1 | | | -0.20 | |
| 904 | EN12607-1 | 61.4 | | -1.07 | |
| 1011 | EN12607-1 | 62 | | -0.90 | |
| 1016 | EN12607-1 | 65.2174 | | 0.00 | |
| 1026 | | 80 | R(0.01) | 4.14 | |
| 1040 | | | | | |
| 1108 | EN12607-1 | 71.7 | | 1.82 | |
| 1135 | EN12607-1 | 64 69 9 | | -0.34 | |
| 1402 | EN12007-1 EN12607-1 | 00.0 70 | | 1.00 | |
| 1613 | D2872 | 62.5 | | -0.76 | |
| 1631 | EN12607-1 | 66 | | 0.22 | |
| 1724 | | 61.4 | | -1.07 | |
| 1730 | EN12607-1 | 60.9 | | -1.21 | |
| 1833 | | 67 | | 0.50 | |
| 1849 | EN12607-1 | 65.1 | | -0.03 | |
| 1852 | EN12607 1 | | | | |
| 1007 | EN 12007-1 | 01.9 | | -0.93 | |
| 1944 | EN12607-1 | 58 53 | | -1.87 | |
| 1990 | | | | | |
| 6037 | | | | | |
| 6076 | | | | | |
| 6228 | | | | | |
| 6229 | EN12607-1 | 64 | | -0.34 | |
| 6364 | | 92.9 | C,R(0.01) | 7.75 | first reported: 94.56 |
| 6404 6410 | EN12607-1 | 64 | | -0.34 | |
| 6474 | | | | | |
| 414 | | | | | |
| | normality | ОК | | | |
| | n | 24 | | | |
| | outliers | 2 | | | |
| | mean (n) | 65.212 | | | |
| | st.dev. (n) | 3.4679 | | | |
| | R(calc.) | 9.710 | | | |
| | SI.UEV.(EINT2007-1.14) R(EN12607-1.14) | 3.5714 10 | | | |
| | | 10 | | | |
| | | | | | |
| 100 T | | | | | U.14 |
| 95 T | | | | | x 0.12 - |



Determination of RTFOT at 163 °C, Viscosity Ratio on sample #22240

| lab | method | value | mark | z(targ) | remarks | |
|----------------|-------------------------|--------|-----------|---------|-----------------------|----------------------|
| 154 | D2872 | 2.77 | С | -1.71 | first reported: 2.766 | |
| 225 | | | | | | |
| 328 | | | | | | |
| 335 | | | | | | |
| 342 | | | | | | |
| 357 | EN12607-1 | 3.0 | | -0.69 | | |
| 360 | | | | | | |
| 365 | | | | | | |
| 396 | | | | | | |
| 390 | | | | | | |
| 444 | | | | | | |
| 447 | | | | | | |
| 604 | | | | | | |
| 657 | D2872 | 3.27 | | 0.51 | | |
| 736 | EN12607-1 | 2.68 | | -2.11 | | |
| 865 | EN12007-1 | 3.17 | | 0.07 | | |
| 904 | | | | | | |
| 1011 | | | | | | |
| 1016 | | | | | | |
| 1026 | | 3.5 | | 1.53 | | |
| 1040 | | | | | | |
| 1135 | EN12607-1 | 34 | | 1 09 | | |
| 1378 | | | | | | |
| 1402 | EN12607-1 | 3.2 | | 0.20 | | |
| 1613 | | | | | | |
| 1631 | | | | | | |
| 1724 | | | | | | |
| 1833 | | | | | | |
| 1849 | | | | | | |
| 1852 | | | | | | |
| 1857 | EN12607-1 | 4.42 | C,G(0.05) | 5.62 | first reported: 0.227 | |
| 1881 | | | | | | |
| 1944 | | | | | | |
| 1990 6037 | | | | | | |
| 6076 | | | | | | |
| 6228 | | | | | | |
| 6229 | | | | | | |
| 6364 | | | | | | |
| 6404 | EN12607-1 | 3.4 | | 1.09 | | |
| 6419 6474 | | | | | | |
| 0474 | | | | | | |
| | normality | OK | | | | |
| | n | 9 | | | | |
| | outliers | 1 | | | | |
| | mean (n) | 3.154 | | | | |
| | st.dev. (n) R(calc.) | 0.2856 | | | | |
| | st.dev.(EN12607-1:14) | 0.2253 | | | | |
| | R(EN12607-1:14) | 0.6319 | | | | |
| | | | | | | |
| ⁵ T | | | | | | 1.6 |
| | | | | | | 1.4 - Kernel Density |
| 4.0 † | | | | | x | 1.2 - |
| 4 - | | | | | | |
| | | | | | | |
| 3.5 + | | | ٨ | ۵ | ۵ | |
| 3 | ۵۵ | . Δ | | | | 0.6 - |
| <u>م</u> | ۵ | | | | | 0.4 |
| 2.5 | | | | | | |
| 2 | | | | | | |
| 736 | 35.7 154 | 1402 | 657 | 135 | 6404 1026 1857 | 0 2 4 6 |

Determination of RTFOT at 163 °C, Increase in Softening Point on sample #22240; results in °C

| lab | method | value | mark | c z(targ) | remarks |
|----------------|------------------------|-------------|-------|----------------|-----------------------|
| 154 | D2872 | 4.6 | С | -1.73 | first reported: 4.8 |
| 225 | | | | | |
| 328 | | | | | |
| 335 335 | | | | | |
| 342 | | | | | |
| 357 | EN12607-1 | 6.6 | | -0.33 | |
| 360 | EN12607-1 | 7.00 | | -0.05 | |
| 365 | | | | | |
| 396 | EN12607-1 | 6.6 | | -0.33 | |
| 390 399 | | | | | |
| 444 | | | | | |
| 447 | | | | | |
| 604 | | | | | |
| 657 | D2872 | 7.0 | | -0.05 | |
| /36 | EN12607-1 | 7.0 | | -0.05 | |
| 701 865 | EN12007-1 | 0.Z | | -0.01 | |
| 904 | FN12607-1 | 6.6 | | -0.33 | |
| 1011 | EN12607-1 | 8.6 | | 1.07 | |
| 1016 | EN12607-1 | 8.2 | | 0.79 | |
| 1026 | | 8.6 | | 1.07 | |
| 1040 | | | | | |
| 1100 | EN12607-1 | 1.3 7.6 | | 0.10 | |
| 1378 | FN12607-1 | 8.1 | | 0.72 | |
| 1402 | EN12607-1 | 7.6 | | 0.37 | |
| 1613 | D2872 | 5.6 | | -1.03 | |
| 1631 | EN12607-1 | 6.7 | | -0.26 | |
| 1724 | | 7 | | -0.05 | |
| 1/30 | EN12607-1 | 6.8 7.0 | | -0.19 | |
| 1849 | FN12607-1 | 7.2 7.3 | | 0.05 | |
| 1852 | LN12007 1 | | | | |
| 1857 | EN12607-1 | 9.22 | | 1.50 | |
| 1881 | | | - | | |
| 1944 | EN12607-1 | 4.8 | С | -1.59 | first reported: 9.8 |
| 1990 6037 | | | | | |
| 6076 | | | | | |
| 6228 | | | | | |
| 6229 | EN12607-1 | 7.8 | | 0.51 | |
| 6364 | | | | | |
| 6404 | EN12607-1 | 6.8 | | -0.19 | |
| 6419 6474 | | | | | |
| | | | | | |
| | normality | OK | | | |
| | n | 25 | | | |
| | outliers | 0 | | | |
| | mean (n) st dev (n) | 1.07 | | | |
| | R(calc.) | 3.02 | | | |
| | st.dev.(EN12607-1:14) | 1.429 | | | |
| | R(EN12607-1:14) | 4 | | | |
| | | | | | |
| ¹² | | | | | |
| 10 | | | | | 0.45 - Kernel Density |
| | | | | | |
| 8 - | | | | · • • | |
| | | Δ Δ Δ | | <u></u> | |
| ۱ ^۲ | ۵ | | | | 0.25 |
| 4 | | | | | |
| , | | | | | 0.1 |
| - T | | | | | 0.05 |
| 0 7 2 2 | <u> </u> | 27 <u>8</u> | 21 8 | <u>z 5 8 6</u> | |
| ÷ 5 | 9 K K K K K | 4 6 F | - 6 1 | 5 8 F 8 | |

Determination of Softening Point (Ring and Ball) on sample #22240; results in °C

| lab | method | value | mark | z(targ) | remarks |
|-----------------|--------------------|--------------|---------------|------------------|----------------------|
| 154 | D36 | 54.0 | С | -0.10 | first reported: 58.8 |
| 225 | D36 | 53.0 | | -1.50 | |
| 328 | EN1427 | 54.2 | | 0.18 | |
| 333 | EN1427 | 53.6 | | -0.66 | |
| 335 | EN1427 | 54.4 | | 0.46 | |
| 34Z | EN 1427 | 53.8 | | -0.38 | |
| 360 | EN 1427 EN 1427 | 04 53.6 | | -0.10 | |
| 365 | EN 1427 EN 1427 | 53.0 | | -0.00 | |
| 396 | EN1427 | 54.2 | | 0.18 | |
| 398 | EN1427 | 54.0 | | -0.10 | |
| 399 | EN1427 | 54.6 | | 0.74 | |
| 444 | EN1427 | 53.7 | | -0.52 | |
| 447 | EN1427 | 53.6 | | -0.66 | |
| 604 | D36 | 54.3 | | 0.32 | |
| 657 | D36 | 55.2 | | 1.58 | |
| 736 | EN1427 | 53.6 | | -0.66 | |
| /81 | EN1427 | 54.6 | | 0.74 | |
| 865 | EN14407 | | | | |
| 904 1011 | EN 1427 EN 1427 | 58.0 | R(0.01) | 5.50 | |
| 1011 | EN1427 EN1427 | 53.8 | | -0.10 | |
| 1010 | EN1427 | 55.2 | | -0.50 | |
| 1020 | EN1427 | 53 10 | | -1.36 | |
| 1108 | EN1427 | 53.7 | | -0.52 | |
| 1135 | EN1427 | 53.6 | | -0.66 | |
| 1378 | EN1427 | 53.8 | | -0.38 | |
| 1402 | EN1427 | 54.0 | | -0.10 | |
| 1613 | D36 | 56.4 | R(0.05) | 3.26 | |
| 1631 | EN1427 | 54.4 | | 0.46 | |
| 1724 | D36 | 54.6 | | 0.74 | |
| 1730 | EN1427 | 54.4 | | 0.46 | |
| 1833 | EN1427 | 55.4 | | 1.86 | |
| 1049 | EN 1427 EN 1427 | 53.5 54.9 | | -1.00 | |
| 1857 | EN 1427 EN 1427 | 53.03 | | -0.20 | |
| 1881 | EN1427 | 52 20 | R(0.05) | -2.62 | |
| 1944 | EN1427 | 54.6 | 11(0.00) | 0.74 | |
| 1990 | D36 | 56.1 | R(0.05) | 2.84 | |
| 6037 | | | 、 | | |
| 6076 | EN1427 | 53.6 | | -0.66 | |
| 6228 | EN1427 | 54.2 | | 0.18 | |
| 6229 | EN1427 | 53.2 | | -1.22 | |
| 6364 | D36 | 56.1 | R(0.05) | 2.84 | |
| 6404 | EN1427 | 54.8 | | 1.02 | |
| 6419 6474 | EN 1427 | 54.3 | | 0.32 | |
| 0474 | | | | | |
| | normality | ОК | | | |
| | n | 39 | | | |
| | outliers | 5 | | | |
| | mean (n) | 54.073 | | | |
| | st.dev. (n) | 0.5719 | | | |
| | R(calc.) | 1.601 | | | |
| | st.dev.(EN1427:15) | 0.7143 | | | |
| | R(EN1427:15) | 2 | | | |
| compar | e R(D36:14P20) | 547 | automated of | ectronic the | ermometer |
| | R(D36:14R20) | 5.47 | mercury there | nometer | |
| | N(B30.14N20) | 0.10 | mercury men | nometer | |
| 50 - | | | | | 0.8 |
| .a [| | | | | Kernel Density |
| 58 + | | | | | x 0.7 |
| 57 | | | | | 0.6 |
| 56 - | | | | | <u> </u> |
| 55 | | | | | |
| | | | | <u>م م م م م</u> | ▲ 0.4] |
| ²⁴ † | | | | | 0.3 - |





Δ

53

Determination of Solubility in Xylene on sample #22240; results in %M/M

| lab | method | value | mark | z(targ) | remarks |
|-----------------|-----------------------|------------------|---|----------------|--|
| 154 | | | | | |
| 225 | | | | | |
| 328 | | | | | |
| 333 | | | | | |
| 342 | EN12592 | 99 99 | | 2 17 | |
| 357 | | | | <u> </u> | |
| 360 | EN12592 | 99.80 | | -1.38 | |
| 365 | | | | | |
| 396 | | | | | |
| 398 | | | | | |
| 399 | | | | | |
| 444 447 | | | | | |
| 604 | | | | | |
| 657 | | | | | |
| 736 | | | | | |
| 781 | EN12592 | 99.77 | | -1.94 | |
| 865 | | | | | |
| 904 1011 | EN12592 | 99.87 | | -0.07 | |
| 1011 | EN 12092 EN 12502 | 99.90 00 0135 | | 0.49 | |
| 1026 | EN 12332 | | | | |
| 1040 | | | | | |
| 1108 | | | | | |
| 1135 | EN12592 | 99.90 | | 0.49 | |
| 1378 | EN12592 | 99.94 | C | 1.23 | first reported: 99.6 |
| 1402 | EN12592 | 99.60 | G(0.01) | -5.11 | |
| 1013 1631 | EN112502 | 00 0 | | 0.40 | |
| 1724 | EN12092 EN12592 | ୬୬.୬ ବଦ ୫୫ | | 0.45 | |
| 1730 | | | | | |
| 1833 | EN12592 | 99.90 | | 0.49 | |
| 1849 | EN12592 | 99.864 | | -0.19 | |
| 1852 | | | | | |
| 1857 | EN12592 | 99.805 | | -1.29 | |
| 1001 | EN112502 | 00 01 | C | | first reported QQ 21 |
| 1990 | EN 12392 | 99.91 | C | | list reported 99.5 r |
| 6037 | | | | | |
| 6076 | | | | | |
| 6228 | | | | | |
| 6229 | EN12592 | 99.82 | | -1.01 | |
| 6364 | | | | | |
| 6404 6410 | EN12592 | 99.82 | | -1.01 | |
| 6474 | | | | | |
| | | | | | |
| | normality | OK | | | |
| | n | 16 | | | |
| | outliers | 1 | | | |
| | mean (n) | 99.874 | | | |
| | st.dev. (n) | 0.0580 | | | |
| | R(calc.) | 0.162 | | | |
| | R(EN12592.14) | 0.0530 | | | |
| | N(LIN12002.14) | 0.10 | | | |
| 100.1 - | | | | | 8 |
| | | | | | Kernel Density |
| 100 - | | | | | |
| 99.9 - | | | | Δ Δ | |
| | 4 | Δ . | <u>, </u> | | 5 - |
| 99.8 - | A | | | | |
| 99.7 - | | | | | |
| 99.6 - x | | | | | |
| | | | | | 2 |
| 99.5 - | | | | | |
| 99.4 | - 0 × 0 | 4 0 - | t 4 - | ω - | |
| 140: | 78 185: 36 6221 | 184 | 2 10 10 | 163 | ឌ្ឌ រដ្ឋ ច្នុំ ^{រដ្} ថ ^{រដ្ឋ} 99.4 99.6 99.8 100 100.2 |

Determination of Ductility on sample #22240; results in cm

| lab | method | value | mark | z(targ) | remarks |
|------|----------|-------|------|---------|--------------------------------------|
| 154 | | | | | |
| 225 | | | | | |
| 328 | | | | | |
| 333 | | | | | |
| 335 | | | | | |
| 342 | | | | | |
| 357 | | | | | |
| 360 | | | | | |
| 365 | | | | | |
| 396 | D113 | 150+ | | | |
| 398 | | | | | |
| 399 | | | | | |
| 444 | | | | | |
| 447 | | | | | |
| 604 | | | | | |
| 657 | D113 | 150+ | | | |
| 736 | D113 | 150+ | | | |
| 781 | D113 | >100 | | | |
| 865 | | | | | |
| 904 | D113 | >100 | | | |
| 1011 | | | | | |
| 1016 | | | | | |
| 1026 | EN13589 | 16.4 | | | possible false negative test result? |
| 1040 | | | | | 1 5 |
| 1108 | | | | | |
| 1135 | D113 | >150 | | | |
| 1378 | | | | | |
| 1402 | | | | | |
| 1613 | D113 | 150 | | | |
| 1631 | | | | | |
| 1724 | | | | | |
| 1730 | | | | | |
| 1833 | | | | | |
| 1849 | | | | | |
| 1852 | | | | | |
| 1857 | | | | | |
| 1881 | | | | | |
| 1944 | | | | | |
| 1990 | | | | | |
| 6037 | | | | | |
| 6076 | | | | | |
| 6228 | | | | | |
| 6229 | D113 | 150+ | | | |
| 6364 | D113 | >100 | | | |
| 6404 | EN13589 | > 150 | | | |
| 6419 | | | | | |
| 6474 | | | | | |
| | | | | | |
| | n | 10 | | | |
| | mean (n) | >100 | | | |

APPENDIX 2

Number of participants per country

1 lab in ALBANIA

- 1 lab in AUSTRIA
- 1 lab in BELGIUM
- 1 lab in BULGARIA

1 lab in CHINA, People's Republic

- 1 lab in COTE D'IVOIRE
- 1 lab in FINLAND
- 3 labs in FRANCE
- 2 labs in GERMANY
- 3 labs in GREECE
- 1 lab in IRELAND
- 4 labs in ITALY
- 1 lab in JORDAN
- 1 lab in KAZAKHSTAN
- 1 lab in KENYA
- 1 lab in LITHUANIA
- 2 labs in MALAYSIA
- 4 labs in NETHERLANDS
- 1 lab in PORTUGAL
- 1 lab in ROMANIA
- 2 labs in RUSSIAN FEDERATION
- 1 lab in SAUDI ARABIA
- 1 lab in SINGAPORE
- 1 lab in SPAIN
- 5 labs in TURKEY
- 4 labs in UNITED KINGDOM
- 1 lab in UNITED STATES OF AMERICA

APPENDIX 3

Abbreviations

| С | = final test result after checking of first reported suspect test result |
|----------|--|
| D(0.01) | = outlier in Dixon's outlier test |
| D(0.05) | = straggler in Dixon's outlier test |
| G(0.01) | = outlier in Grubbs' outlier test |
| G(0.05) | = straggler in Grubbs' outlier test |
| DG(0.01) | = outlier in Double Grubbs' outlier test |
| DG(0.05) | = straggler in Double Grubbs' outlier test |
| R(0.01) | = outlier in Rosner's outlier test |
| R(0.05) | = straggler in Rosner's outlier test |
| E | = calculation difference between reported test result and result calculated by iis |
| W | = test result withdrawn on request of participant |
| ex | = test result excluded from statistical evaluation |
| n.a. | = not applicable |
| n.e. | = not evaluated |
| n.d. | = not detected |
| fr. | = first reported |
| f+? | = possibly a false positive test result? |
| f-? | = possibly a false negative test result? |
| SDS | = Safety Data Sheet |

Literature

- 1 iis Interlaboratory Studies, Protocol for the Organisation, Statistics & Evaluation, June 2018
- 2 ISO5725:86
- 3 ISO5725 parts 1-6:94
- 4 ISO13528:05
- 5 M. Thompson and R. Wood, J. AOAC Int, <u>76</u>, 926, (1993)
- 6 W.J. Youden and E.H. Steiner, Statistical Manual of the AOAC, (1975)
- 7 P.L. Davies, Fr. Z. Anal. Chem, <u>331</u>, 513, (1988)
- 8 J.N. Miller, Analyst, <u>118</u>, 455, (1993)
- 9 Analytical Methods Committee, Technical Brief, No 4, January 2001
- 10 P.J. Lowthian and M. Thompson, The Royal Society of Chemistry, Analyst, <u>127</u>, 1359-1364, (2002)
- 11 W. Horwitz and R. Albert, J. AOAC Int, <u>79.3</u>, 589-621, (1996)
- 12 Bernard Rosner, Percentage Points for a Generalized ESD Many-Outlier Procedure, Technometrics, <u>25(2)</u>, 165-172, (1983)